

## Original Research Article

### IMPROVEMENT OF THREE PHASE INDUCTION MOTOR PERFORMANCE USING VOLTAGE AND FREQUENCY SPEED CONTROL TECHNIQUES

#### ABSTRACT

Induction motors are the most widely used electrical motors due to their reliability, low cost and robustness. However, induction motors do not inherently have the capability of variable speed operation. Due to this reason, earlier dc motors were applied in most of the electrical drives. The Advent of power electronics has drastically made a lot of improvement, where alternating current drive is used to run and control the performance of induction motor. This research work presents the use of voltage and Frequency control technique to enhance the performance of speed control of three phase induction motor. Controlling the speed of motor using traditional method such as controlling the supply voltage ,changing the stator pole and others incures running motor at full speed ,speed instability, and the efficiency of the motor drop when motor speed is varied but the voltage and frequency ratio method of speed control solves this problem .A model and simulation in MATLAB for various method of speed control was analysed with constant voltage and frequency method showing much improvement on the speed and electromagnetic torque characteristic of the induction motor compared to other method such as change in stator resistance ,rotor resistance, number of poles, stator leakage resistance and others. Varying the line frequency at a maintained constant 8V/Hz V/F ratio and the effect of the torque-speed characteristics performance of the three-phase induction motor for line frequencies were investigated: (40Hz, 50Hz, 60Hz, 70Hz, and 80Hz). The result shows that as the line frequency increases, the torque decreases and the speed increases (or slip decreases), and for a line frequency of 40Hz, the torque observed is 43.6Nm while the rotor speed is 1076rpm. But for a line frequency of 80Hz, the peak torque was observed at 22Nm while the corresponding rotor speed was 2152rpm, thereby enhancing the speed control performances of the three-phase induction motor and its voltage frequency characteristics.

**Key Words:** induction motor; Matlab; Improvement; Supply Voltage; Frequency Variation; Speed Control; sensorless; V/F ratio; Cyclo Converter; Stator and Rotor.

#### INTRODUCTION

Three-phase induction motor drives are employed in several industrial areas with a good power, ranging from few 100W to many MW. In industrial-oriented countries, more than half the total

electrical energy used is converted to mechanical energy through AC induction motors. Induction motors have industrial and household applications and expend over 50% of the total generated electrical energy. Induction motor (three phase) popularity on board ship is due to their high reliability factor simplicity in design, robustness in construction, low cost and high efficiency. Different application can be used by three phase induction motor with their various load requirement and speed, and its significant is to ensure cost effective operation [1]. Single phase induction motors are widely utilized in home appliances and industrial control. During the last few years, speed and torque control principle are asynchronous with motor drives which gained significant popularity. It is possible to combine the induction-motor structural robustness with the control simplicity and efficiency of a direct current motor. This evolution resulted to the replacement of the dc machines by induction motors in many applications in the last few years. Earlier only dc motors were employed for drives requiring variable speeds due to facilities of their speed control methods [2].

The conventional methods of speed control in an induction motor are very expensive or too inefficient thus restricting their level of application to only constant speed drives. Examples include driving pumps, fans, compressors, mixers, agitators, mills, conveyors, crushers, machine tools and cranes. They are very simple, reliable, low maintenance and low cost. Today, with advancements in power electronics, microcontrollers, and digital signal processors (DSPs), electric drive systems have improved drastically. Initially the principle of speed control was based on steady state consideration of the induction motor. Voltage and frequency control was suitable for the open-loop speed control of drives with low dynamic requirements. Several techniques of induction motor speed control have been developed; these include: pole changing, frequency variation, variable rotor resistance, variable stator voltage, constant V/f control, slip recovery method etc. Controlling the speed of a motor using traditional methods involve running the motor at full speed and then using mechanical means such as gears, hydraulic couplings or pulleys. This is not only expensive, but also consumes tons of energy when there are many means of controlling induction motor speed. The most popular problem discovered in them is that motor used to experience speed instability and the efficiency of the motor drops when the motor speed is varied. There are different methods of controlling induction motor for industrial application. Voltage and frequency ratio method offers an easy way to regulate both the frequency and magnitude of the voltage applied to a motor. However, better efficiency can be obtained by these motor drives with less noise. The most rampant technique is the constant Voltage and frequency principle which requires that frequency and the magnitude of the voltage applied to the stator of a motor maintain a constant ratio. So, by this, the magnetic field in the stator is kept almost constant for all operating points. Thus, constant torque is maintained. The aim of this research work is to enhance the performance and efficiency of speed control of three phase induction motor using voltage and frequency ratio method. It also explained the best techniques for controlling the speed of electric motor and designed to be of immense benefit to all the users of electric motor most especially in industries and serve as a useful piece of information for both producers and users of electric motor speed controller.

## 2. THE USE OF INDUCTION MOTOR

In modern countries, more than half the electricity used is converted to energy through induction motors. Induction motors are extensively utilized in industrial and household appliances and consume more than 50% of the entire generated electricity. Single-phase induction motors are widely utilized in home appliances and industrial control. During the previous couple of years, the concept of speed and torque control of asynchronous motor drives has gained significant popularity. This way, it's been possible to mix the induction-motor structural robustness with the control simplicity and efficiency of an immediate current motor. This evolution resulted to the replacement of the direct current machines with induction motors in many applications within the previous couple of years. Earlier only dc motors were employed for drives requiring variable speeds due to facility of their speed control methods.

Speed control of an induction motor were either too extravagant thus limiting their application to only constant speed drives. They are used to drive pumps, fans, compressors, mixers, agitators, mills, conveyors, crushers, machine tools, cranes, etc. sort of electrical motor is so popular thanks to its simplicity, reliability, less maintenance and low cost. Today, with advancements in power electronics, microcontrollers, and digital signal processors (DSPs), electric drive systems have improved drastically. Consideration of the induction motor, V/F control was the commonly used method for the open-loop speed control of drives with low dynamic requirements which is the focus of this research work.

Replacement of current-limiting soft-starter for a three-phase induction motor drive system using pulse width modulation (PWM) chopper unique in configuration with three-phase has been presented [3] A good AC-chopper using only four insulated gate bipolar transistors (IGBTs) is additionally proposed. It requires just one current sensor. The duty ratio of the chopper IGBTs from the closed loop current control so as to limit the motor starting current at a preset value. Only two complementary gate pulses are obtained from the negative feedback circuit to regulate the four IGBT switches. Posit that phased two-level inverters voltage space vector for the three-level inverter-controlled induction motor with cascades [4]. This study proposes a five-level torque controller (FLTC)-based torque control technique to boost steady-state motor torque performance and retaining the high dynamic performance.

The quality field oriented control (FOC) for induction motors (IM) is that the finite control set model predictive control (FCS-MPC) presented the foremost serious and up to date competitor [5], the study shows that Direct torque control (DTC) has been widely used as an alternate to traditional field-oriented control (FOC) methods for three-phase drives. They also suggested that Direct torque control (DTC) has been recently used for the event of high efficiency in five-phase induction motor (IM) drives. This work analyzes the fault-tolerant capability of six-phase drives with parallel converter supply. Scenarios of up to 3 faults for single and two neutral configurations are examined, optimizing off-line the post-fault currents and modifying accordingly the control strategies. Has evaluated a model to control scheme for multiphase induction machines with multi three-phase. Complete details about the predictive control scheme and adopted flux observer are included, has been suggested

Direct torque control (DTC) has been recently used for the event of high performance five-phase induction motor (IM) drives in normal operation of the system and therefore the ability of DTC to manage things has been analyzed as compared with different rotor field-oriented control (RFOC) strategies [6], discussed Three-phase machines are the industry standard for electrical drives, but the inherent fault tolerance of multiphase machines makes them a beautiful alternative in applications requiring high reliability. This novel strategy is then combined with minimum losses and maximum torque criteria to urge a variable current injection method that minimizes the drive derating, reduces the copper losses and improves the braking transients. It was observed that the six-phase induction motor drive can perform successfully within the different zones.

The reviewed high order and nonlinearity of the dynamics of an induction motor, estimation of the angle speed and rotor position without the measurement of mechanical variables becomes a challenging problem [7]. The benefits of position and more so speed of a sensorless induction motor drives are to reduced hardware complexity and lower cost, reduce size of drive machine, eliminate of sensor cable, better noise immunity, increasing reliability and fewer maintenance requirements. The presentation of sliding mode controller with rotor flux estimation for induction motor drives [8, 9], the rotor flux was also estimated using a sliding mode observer. Most methods are basically supported the Model Reference Adaptive System schemes (MRAS). Confirmed reactive-power-based-reference model was confirmed and derived in both motoring and generation modes but one among the disadvantages of this algorithm is its sensitivity to detuning within the stator and rotor inductances [10] An MRAS pattern is so simple but its greatest drawback is that the sensitivity to uncertainties within the motor parameters.

Another method based on the Extended Kalman Filter (EKF) algorithm was proposed [11]. The EKF may be a stochastic state observer where nonlinear equations are linearized in every sampling period. An interesting feature of the EKF is its ability to estimate simultaneously the states and therefore the parameters of a dynamic process. This is generally useful for both the control and therefore the diagnosis of the method.

The advances in microprocessor and power electronics which provides permission to implement modern techniques for induction machines like field-oriented control also referred to as vector control [12]. This provides higher efficiency; lower operating costs and reduces the value of drive components. In sensor-less field with oriented control, the speed or position cannot be estimated, their values are estimated using other parameters like phase voltages and current, that are directly measured. Sensorless drives are getting more and more important as they will eliminate speed sensors maintaining accurate response. While observing only the stator current and voltages, it is possible to estimate the necessary control variables. There is other sort of methods for state estimation that's supported the intelligent techniques is employed within the recent years by many authors. The discussion Variable-speed constant- frequency generating systems are used in wind power, hydro power, and aerospace and naval power generations to enhance efficiency and reduce friction [13]. In these applications, the slip power recovery system comprising of doubly excited induction machine or doubly excited brushless reluctance machine and PWM converters with a dc

link. Thus from the working rule of three phase induction motor, it's going to be observed that the rotor speed shouldn't reach the synchronous speed produced by the stator. If the speeds become equal, there would be no such relative speed, so no EMF induced within the rotor, and no current would be flowing, and thus no torque would be generated. Consequently, the rotor cannot reach the synchronous speed. The difference between the stator (synchronous speed) and rotor speeds is named the slip. The rotation of the magnetic flux in an induction motor has the advantage that no electrical connections got to be made to the rotor.

### 3. METHODOLOGY

The data used for this research work comprises of machine parameters gotten from Cummins induction motor manufacturer, Vein Road Onitsha, between January and April 2019 as shown in Table 1. The simulation sequence of the developed models for the three-phase induction motors in Matlab is given in the flow sequence take to write a program in a scalar non-interactive language as shown in Figure 1. The simulation sequence was modelled and developed in Matlab using equation (3.38). Nine (9) script files and codes were written to accommodate the nine sensitivity analyses performed on the investigation of the effect of changing parameters on the three-phase induction motors. Figure 4, 5, 8 and 9 shows the effect of varying supply voltage, line frequency, frequency at constant V/F ratio and frequency at varied V/F ratio of the torque-speed characteristics performance of the three-phase induction motor. Figure 2 and 3 shows the hardware design and implementation.

From Figure 2, TR<sub>1</sub> is as step down transformer from 315v to 12V, BR<sub>1</sub> is bridge rectifier which rectifies the out coming voltage from tr<sub>1</sub>, c<sub>1</sub> filter the rectified voltage, R<sub>1</sub> and R<sub>2</sub> forms a voltage divider, this sub circuit create a power supply to the microcontroller which is used to control V/F of the induction motor. Also from Figure 3, the main of 220V a.c passes through bridge rectifier BR<sub>2</sub> which rectifies the incoming a.c into a pulsating dc. C<sub>2</sub> filters the rectified voltage form BR<sub>2</sub>. TR<sub>1</sub> is a step-down transformer, which steps down the main of 220V to 230v into 12V a.c, BR<sub>1</sub> rectifies the 12V ac form TR<sub>1</sub> into pulsating d.c C<sub>1</sub> filters BR<sub>1</sub>. U<sub>1</sub> is 7805 regulator which regulator which regulate the input Dc volt 12V to 5V dc, C<sub>4</sub> filters the regulated voltage to U<sub>2</sub>. U<sub>2</sub> is the heart beat of the control circuits which control the voltage and frequency and also generate pulses to fire U<sub>3</sub>, U<sub>4</sub> and U<sub>5</sub>. U<sub>2</sub> pin 15 and pin 16 is connected to a crystal oscillator which oscillates at 20MHz driving U<sub>2</sub> into oscillation. U<sub>2</sub> pin 2, pin 3, pin 8 and pin 9 are used for controlling the frequency and voltage. U<sub>3</sub>, U<sub>4</sub>, and U<sub>5</sub> are opta isolated drivers. R<sub>7</sub>, R<sub>8</sub> and R<sub>9</sub> are current limiter which protects U<sub>3</sub> to U<sub>4</sub> from excess current. V<sub>6</sub>, V<sub>7</sub> and V<sub>8</sub> are power amplifiers which amplify the signal form U<sub>3</sub>, U<sub>4</sub> and U<sub>5</sub> to the induction motor.

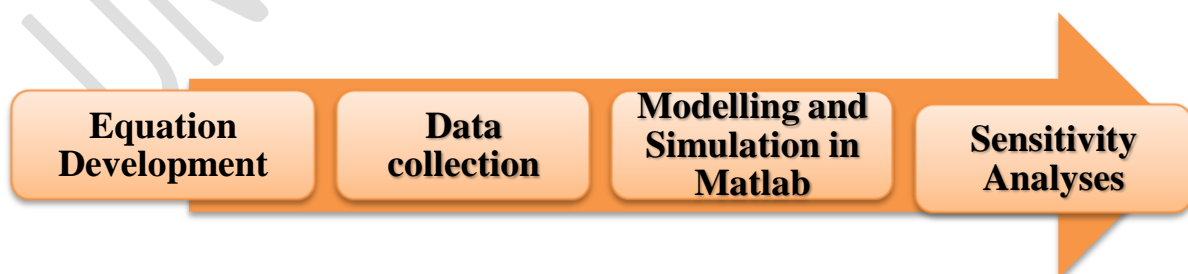


Figure 1: Block Diagram of Flow Sequence



Parameter	Value	
	Base	Sensitivity
Line to Line supply voltage (RMS value)	400 V	400V, 440V, 480V, 520V, 560V
Stator Resistance	0.1 ohm	0.1ohm, 0.15ohm, 0.2ohm, 0.25ohm, 0.3ohm
Rotor Resistance	0.15 ohm	0.15ohm, 0.2ohm, 0.25ohm, 0.3ohm, 0.35ohm
Number of poles	4	4, 6, 8, 10, 12
Frequency	50 Hertz	40 Hertz, 50 Hertz, 60 Hertz, 70 Hertz, 80 Hertz
Stator leakage resistance @ 50 Hz	0.75 ohm	0.55ohm, 0.65ohm, 0.75ohm, 0.85ohm, 0.95ohm
Rotor leakage resistance @ 50 Hz	0.75	0.55ohm, 0.65ohm, 0.75ohm, 0.85ohm, 0.95ohm
V/F ratio	8 V/Hz	6V/Hz, 7V/Hz, 8V/Hz, 9V/Hz, 10V/Hz
Power Rating	1.8 kw	

#### 4. INDUCTION MOTOR SPEED CONTROL TECHNIQUES

There are many techniques involve in controlling the speed of induction motor, but here are discussed the techniques related to this research work and they are as follows:

##### 4.1. Speed Control by Varying Supply Voltage

The speed of induction motor can be varied by changing supply voltage. The torque developed during this method is proportional to the square of the availability voltage ( $T \propto V^2$ ). This is the most cost effective and simplest way, but it's rarely used due to the below reasons. A small change in speed requires an outsized change in voltage. This large change in voltage will end in an outsized change within the flux. The torque produced by running three phase induction motor is given by:

$$T \propto \frac{sE_2^2 R_2}{R_2^2 + (sX_2)^2} \quad 1.0$$

$$T \propto \frac{sE_2^2}{R_2} \quad 1.1$$

The low slip region  $(sX)^2$  is extremely small as compared to  $R^2$ . So, it can be neglected. Since rotor resistance,  $R_2$  is constant so the equation of torque further reduces to

$$T \propto sE_2^2 \quad 1.2$$

the rotor induced EMF  $E_2 \propto V$ . So,  $T \propto sV^2$ . The equation above clears that if we decrease supply voltage torque also will decrease. But for supplying an equivalent load, the torque must remain an

equivalent, and it's only possible if we increase the slip and if the slip increases the motor will run at a reduced speed. This method of speed control is never used because a little change in speed requires an outsized reduction in voltage, and hence the present drawn by motor increases, which cause overheating of the induction motor.

#### 4.2. Speed Control by Frequency Variation

Variable Frequency Control is a method which is employed to regulate the speed of an induction motor. The synchronous speed and therefore, the speed of the motor can be controlled by varying the supply frequency. By varying the supply frequency (on small amount), will vary the speed. But a decrease in supply frequency decreases the speed and increases the flux, core losses which lead heating and low efficiency. Increase in frequency increases the speed and reduces the torque. Separate costlier auxiliary equipment is required to provide a variable frequency. The synchronous speed of an induction motor is given by:

$$N_s = \frac{120f}{P} \quad 1.3$$

Where,  $f$  = frequency of the availability and  $P$  = number of stator poles.

Hence, the synchronous speed changes with change in supply frequency. Actual speed of an induction motor is given as

$$N = N_s (1 - s). \quad 1.4$$

Where  $N$  = Actual speed,  $N_s$  = Synchronous speed,  $S$  = Slip.

The EMF induced in the stator of the induction motor is given by the equation in (1.4).

$$E_1 = 4.44k_{w1}f\phi T_1 \quad 1.5$$

Therefore, if the availability frequency is modified induced EMF also will change to take care of an equivalent air gap flux. The terminal voltage  $V_1$  is equal to the induced EMF  $E_1$  if the stator voltage drop is neglected. In order to minimize the losses and to avoid the saturation, the motor is operated at rated air gap flux. This condition is obtained by varying the terminal voltage with frequency so on maintain  $(V/f)$  ratio constant at the speed value. This type of control is understood as Constant Volts per Hertz.

Thus, the speed control of an induction motor using variable frequency supply requires a variable voltage power source. The variable frequency supply is obtained by the subsequent converters such

as: voltage source inverter, current source inverter and cyclo converter. An inverter converts a hard and fast voltage DC to a hard and fast or variable voltage AC with variable frequency. Cyclo converter converts a hard and fast voltage and glued frequency AC to a variable voltage and variable AC frequency. The variable frequency control allows good running and transient performance to be obtained from a cage induction motor. Cyclo converter-controlled induction motor drive is suitable just for large power drives and to urge lower speeds.

### 4.3. Changing the Number of Stator Poles

From the above equation (1.3) of synchronous speed, it can be seen that synchronous speed can be changed by changing the number of stator poles. This method is usually used for cage induction motors, as cage rotor adapts itself for any number of stator poles. Change in stator poles is achieved by two or more independent stator windings wound for various numbers of poles in same slots. For example, a stator is wound with two 3phase windings, one for 4 poles and other for 6 poles for supply frequency of 50 Hz. The synchronous speed when 4 pole winding is connected,  $N_s = 120 \cdot 50 / 4 = 1500$  RPM and the synchronous speed when 6 pole winding is connected,  $N_s = 120 \cdot 50 / 6 = 1000$  RPM.

### 4.4. Control from Rotor

This method involves using rotor rheostat control and by injecting EMF in rotor circuit as follows:

- (a) **Rotor rheostat control;** this method is analogous thereto of armature rheostat control of DC shunt motor. But this method is merely applicable to slip ring motors, as addition of external resistance within the rotor of cage motors isn't possible. Also, in this method of speed control, two motors are used. Both are mounted on a same shaft so that both run at the same speed. One motor is fed from a 3phase supply and therefore the other motor is fed from the induced EMF in first motor via slip-rings as shown in Figure 4.

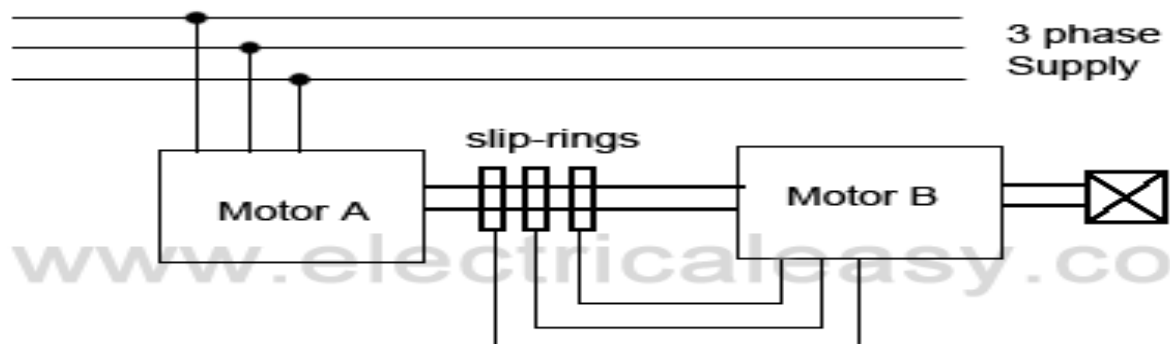


Figure 4: Motor Arrangement.

Motor A is called the main motor and motor B is called the auxiliary motor. Let,  $N_{s1}$  = frequency of motor A,  $N_{s2}$  = frequency of motor B,  $P_1$  = number of poles stator of motor A,

$P_2$  = number of stator poles of motor B,  $N$  = speed of the set and same for both motors and  $f$  = frequency of the supply. Now, slip of motor A,  $S_1 = (N_{s1} - N) / N_{s1}$ .

Frequency of the rotor induced EMF in motor A,  $f_1 = S_1 f$ . Now, auxiliary motor B is supplied with the rotor induce EMF. Therefore,  $N_{s2} = (120f_1) / P_2 = (120S_1 f) / P_2$ .

Now putting the value of  $S_1 = (N_{s1} - N) / N_{s1}$  gives equation (1.6).

$$N_{s2} = \frac{120f(N_{s1} - N)}{P_2 N_{s1}} \quad (1.6)$$

At no load, speed of the auxiliary rotor is almost same as its synchronous speed. i.e.  $N = N_{s2}$ . from equation (1.6) it can be obtained that:

$$N = \frac{120f}{P_1 + P_2} \quad (1.7)$$

With this method, four different speeds can be obtained.

- (i) When only motor A works, corresponding speed =  $N_{s1} = 120f / P_1$ .
- (ii) When only motor B works, corresponding speed =  $N_{s2} = 120f / P_2$ .
- (iii) If commutative cascading is done, speed of the set =  $N = 120f / (P_1 + P_2)$ .
- (iv) If differential cascading is done, speed of the set =  $N = 120f / (P_1 - P_2)$ .

**(b) By injecting EMF in rotor circuit;** in this method, speed of an induction motor is controlled by injecting a voltage in rotor circuit. It is necessary that voltage EMF being injected must have same frequency as of the slip frequency. However, there is no restriction to the phase of injected EMF. If we inject EMF which is in opposite phase with the rotor induced EMF, rotor resistance will be increased. If we inject EMF which is in phase with the rotor induced EMF, rotor resistance will decrease. Thus, by changing the phase of injected EMF, speed are often controlled. The main advantage of this method may be a wide range of speed control (above normal also as below normal) is often achieved. The EMF is often injected by various methods like Kramer system and Scherbius system.

#### 4.5. Sensorless Control Method

Motor drives without a speed or position sensor have received much research attention in recent years, both for induction motors and PM brushless types. Such techniques typically measure stator quantities, usually current, directly via existing transducers normally present within the inverter and voltage, although rarely with an immediate measurement. SI methods are also used. Figure 5 shows a typical schematic of a sensorless scheme and the advantages of sensorless control method schemes include: more compact drive with less maintenance, no cable to machine transducers, easier application particularly to existing machines, reduced electrical noise, transducer cost is

avoided and suitable for hostile environments (temperature). Despite much effort and progress, operation at very low speed remains problematic particularly for an induction motors sensorless drive.

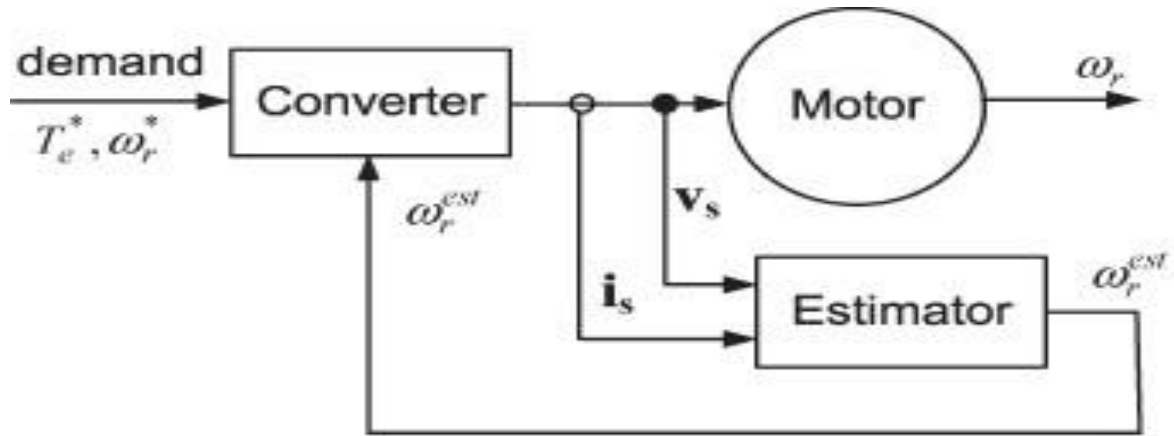


Figure 5: Schematic of a speed sensorless.

#### 4.6. Equation development

Three-phase induction motors are represented by set of equations. The slip is given by

$$S = \frac{N_s - N_r}{N_s} \quad (1.8)$$

Where  $S = \text{slip}$ ,  $N_s = \text{synchronous speed}$ ,  $N_r = \text{Rotor speed}$ .

The rotor speed can otherwise be written as:

$$N_r = N_s(1 - S) \quad (1.9)$$

The Synchronous speed is given as:

$$N_s = \frac{120f}{P}, \quad \text{rpm} \quad (2.0)$$

or

$$N_s = \frac{2f}{P}, \quad \text{rps} \quad (2.1)$$

Where, if the unit of the synchronous speed is to be determined in radians, then the speed has to be multiplied by the factor  $(2\pi)$ .

$$\omega_s = 2\pi N_s \quad (2.2)$$

Similarly, the angular value of the rotor speed is give as:

$$\omega_r = 2\pi N_r \quad (2.3)$$

The rotor current is given as:

$$I_2 = \frac{V_0}{\left[ \left( R_s + \frac{R_r}{S} \right)^2 (X_s + X_r)^2 \right]^{0.5}} \quad (2.4)$$

The electromagnetic torque is given as:

$$T = \left[ \frac{3}{\omega_s} \right] \left[ \frac{R_s}{S} \right] \left\{ \frac{V_0}{\left[ \left( R_s + \frac{R_r}{S} \right)^2 (X_s + X_r)^2 \right]^{0.5}} \right\} \quad (2.5)$$

Where, T is the electromagnetic torque [Nm],  $\omega_s =$  is the synchronous speed, rads/sec.

If the synchronous speed is in revolutions per minute then the torque is given by:

$$T = \left[ \frac{3}{N_s} \right] \left[ \frac{R_s}{S} \right] \frac{V_0}{\left[ \left( R_s + \frac{R_r}{S} \right)^2 (X_s + X_r)^2 \right]^{0.5}} \quad (2.6)$$

The power analyses of the circuit are given as follows: the power transferred across the air gap to the rotor is given as:

$$P_g = 3E_2 I_2 \cos \theta_2 = \frac{3I_2^2 r_2}{S} \quad (2.7)$$

The rotor copper loss is given as:

$$P_{cu} = 3I_1^2 r_1 \quad (2.9)$$

$$P_m = P_g - P_{cu} \quad (3.0)$$

$$P_o = P_m - (\text{Frictional losses, windage and stray losses}) \quad (3.1)$$

Thus, torque is given as:

$$T = \frac{P_m}{\omega_r} = \frac{P_m}{2\pi N_r} \quad (3.2)$$

The torque developed is proportional to the air gap power  $P_g$ . The air gap power  $P_g$  is usually known as torque measured in synchronous watts.

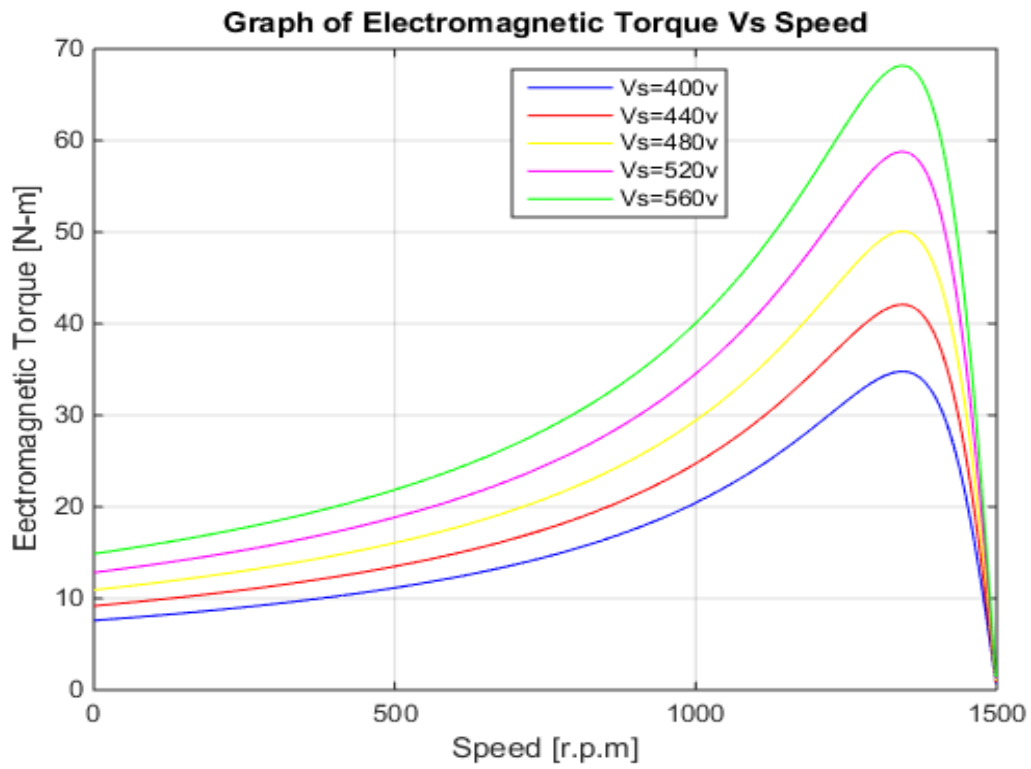


Figure 6: Torque -speed at varied supply voltage

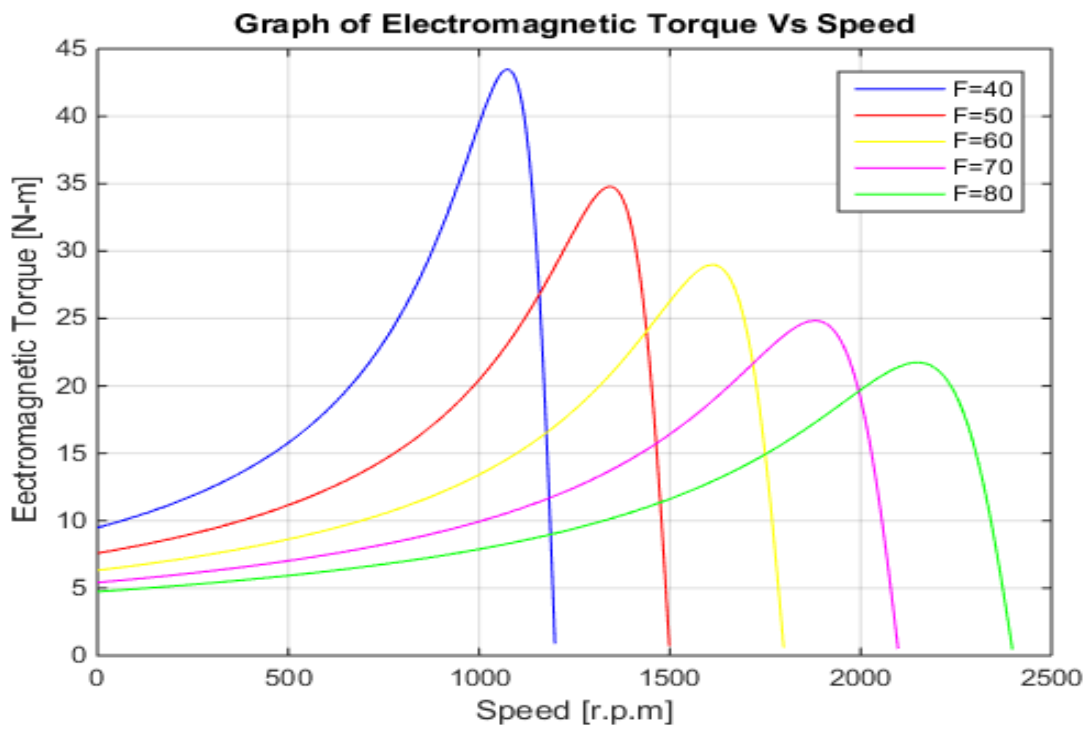


Figure 7: Torque -speed at varied line frequency

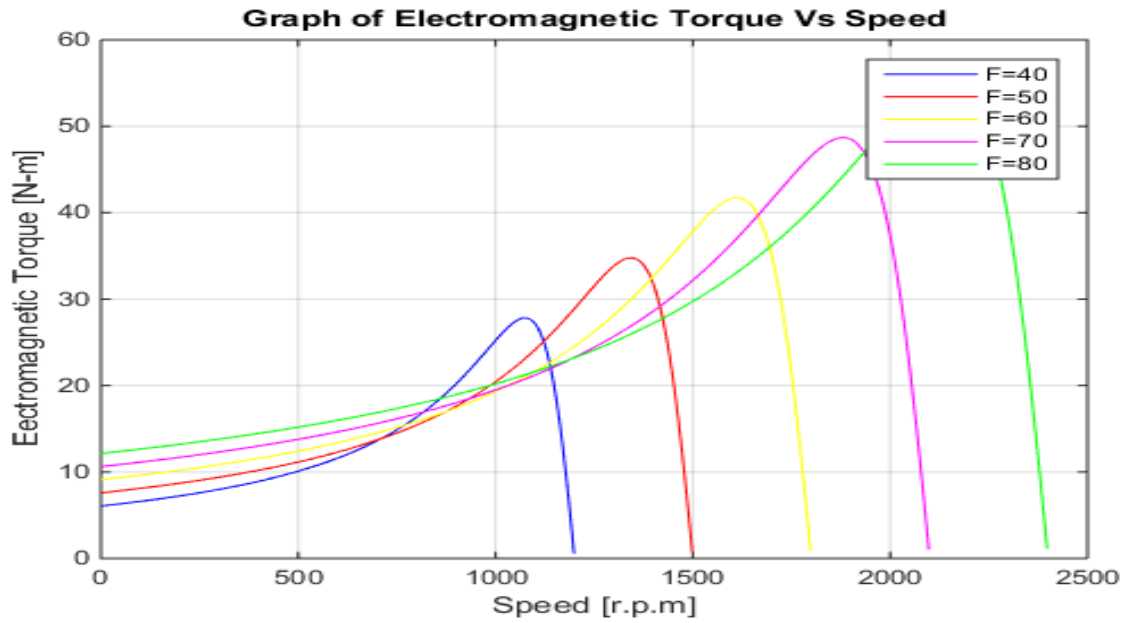


Figure 8: Torque -speed at varied frequency and constant V/F ratio

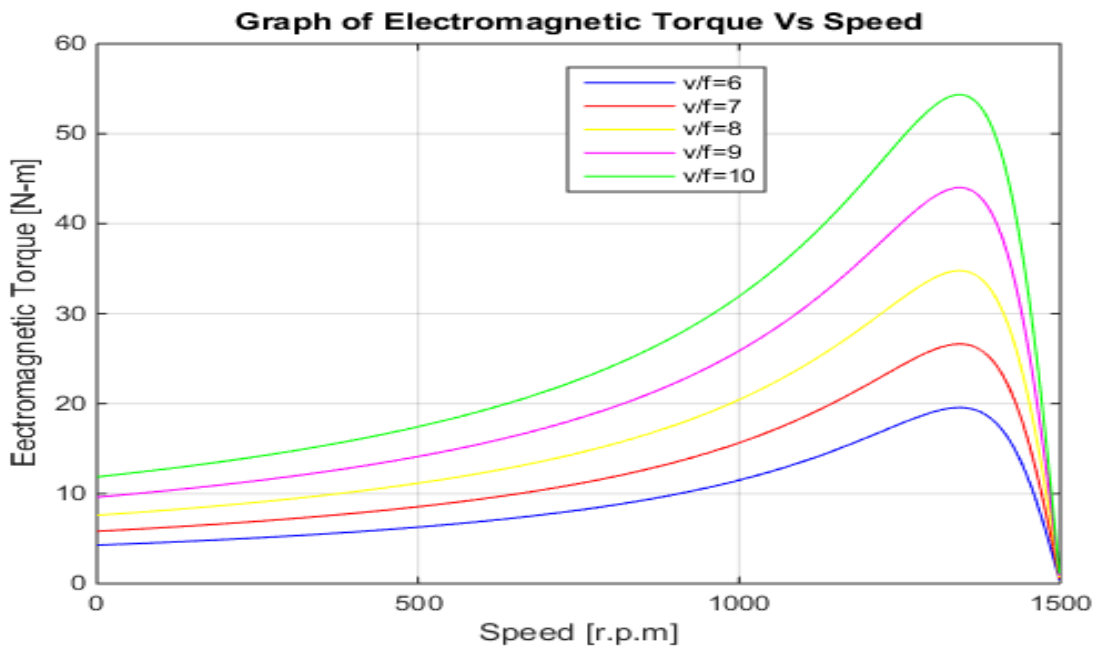


Figure 9: Torque -speed at varied V/F ratio

## 5. RESULTS AND DISCUSSION

The result for the effect of the changing parameters on the torque-speed value for the three-phase induction motors are presented in Figure 4, 5, 8 and 9, and they represent the steady state behaviour

of the three-phase induction motor. The varied supply voltage and the effect of the torque-speed characteristics performance of the three-phase induction motor for line-to-line RMS voltage were investigated: (400V, 440V, 480V, 520V, 560V). It was observed from Figure 4 that as the supply voltage increases, the torque increases and the speed remains constant, and for a voltage of 400V, the torque peaked at 35Nm corresponding to 1350rpm. While for 560V, (green line) the torque peaked at 68.2Nm corresponding to 1350rpm. Thus as the voltage increases, the torque increases while the rotor speed remains constant (i.e. at the same slip). Varying the line frequency at a maintained constant 8V/Hz V/F ratio and the effect of the torque-speed characteristics performance of the three-phase induction motor for line frequencies were investigated: (40Hz, 50Hz, 60Hz, 70Hz, and 80Hz). The result shows that as the line frequency increases, the torque decreases and the speed increases (or slip decreases), and for a line frequency of 40Hz, the torque observed from figure 5 is 43.6Nm while the rotor speed is 1076rpm. But for a line frequency of 80Hz, the peak torque was observed at 22Nm while the corresponding rotor speed was 2152rpm. It was also observed from Figure 8 that as the line frequency increases at constant V/F ratio, the torque increases and the speed also increases (or slip decreases). For a line frequency of 40Hz, the torque observed from figure 8 is 27.9Nm while the rotor speed is 1080rpm. But for a line frequency of 60Hz, the peak torque was observed at 42Nm while the corresponding rotor speed was 1614rpm. Thus increasing the line frequency at constant V/F ration increases the electromagnetic torque and also increases the rotor speed (decreased slip).

The effect of varying V/F ratio as shown in Figure 9 shows that as the V/F ratio increases, the torque increases and the speed remains constant. For V/F ratio of 6V/Hz (the blue line), the torque peaked at 19.8Nm corresponding to 1350rpm. While for 10V/Hz, (green line) the torque peaked at 54.8Nm corresponding to 1350rpm. Thus as the voltage increases, the torque increases while the rotor speed remains constant (i.e. at the same slip). It is pertinent to note that the speed control of the three-phase induction motor was enhanced and the evaluations made herein are geared towards improvements in characteristics of the voltage frequency.

## 6. CONCLUSION

The techniques of constant V/F ratio control, the supply voltage as well as the supply frequency can be varied such that the flux remains constant. So we can get different operating zone for various speeds and torques and this can be achieved at constant flux. Achieving different synchronous speed with almost same maximum torque makes the motor completely utilized and also has a good range of speed control. To maintain the V/F ratio helps us to maintain a constant maximum torque while controlling the speed. It is therefore recommended that the ratio of the change in voltage and frequency must be constant in order to keep the flux content. Thus by maintaining a constant V/f ratio maximum torque of the motor becomes constant for changing speed and the initial starting load torque should be zero. This will make the motor speed to move from the incremented of zero to the synchronous speed.

## 6. REFERENCE

- [1] Saif Alkahim Aldeen. Three Phase Induction Motor: Type and Structure. SSRN Electronic Journal, 2020.
- [2] Zubek J, Abbondanti A, and Norby, C. J, "Pulse width modulate diverter motor drives with improved modulation," IEEE Trans. Ind. Applicat., vol. 11, 2010, Nov./Dec ,pp.695–703.
- [3] A. Deraz and Haitham Z. Azazi1,"Current limiting soft starter for three phase induction motor drive system using PWM AC chopper ",IET Power Electronics.2004, P.34-44.
- [4] Pratibha Naganathan1,SriramaSrinivasandHridayalttamveetil, Five-level torque controller-based DTC method for a cascaded three level inverter fed induction motor drive", IET Power Electron.,© The Institution of Engineering and Technology , Vol. 10. 2017, pp. 1223-1230.
- [5] I.Gonzalez-Prieto, M.J.Duran ,J.J.Aciego, C. Martin, and F.Barrero, "Model Predictive Control of Six-phase Induction Motor Drives Using Virtual Voltage Vectors ",IEEE Transactions On Industrial Electronics, 2005 pp.10-24.
- [6] Mario Bermudez, Ignacio Gonzalez-Prieto, Federico Barrero, Hugo Guzman , Xavier Kestelynland Mario J. Duran, "An Experimental Assessment of Open-Phase Fault-Tolerant Virtual Vector Based Direct Torque Controlin Five-Phase Induction Motor Drives", IEEE Transactions On Power Electronics. 2006, pp.48-57.
- [7] F.A.Toliyat, E. Levi and M. Raina "A Review of RFO Induction Motor Parameter Estimation Techniques", IEEE Trans. on Energy Conversion, Vol. 18, No.2, 2003, June pp.18-11.
- [8] Benchaib, A., A. Rachid, E. Audrezet, and M. Tadjine, "Real time sliding mode observer and control of an induction motor, "IEEE Trans. on Ind. Electronics,vol.46, no.1, 1999, Febuary,pp.128-138.
- [9] Cirrincione M., Pucci M., "Sensorless direct torque control of an induction motor by a TLS-based MRAS observer with adaptive integration," Automatica, vol. 41, 2005 pp. 1843-1854.
- [10] Bilal A., Umit O., Aydin E., Mehrded E., "A Comparative Study on Non- Linear State Estimators Applied to Sensorless AC Drives: MRAS and Kalman Filter," 30 Annual Conf. of the IEEE Ind. Electron. Society .Busan , Korea.vol.11 2004 .pp74-135.
- [11] Ouhrouche M. A., "Estimation of speed, rotor flux and rotor resistance in cage induction motor using the EKF-algorithm," Int. J. Power and Energy system 2000,pp.1-20.
- [12] Negm , Torque optimized speed control of a three phase induction motor", in Proc .Int. Conf. power system technology, 2000 pp. 67-72.
- [13] Yifan Tang , Member , IEEE, and Long yaXu, Senior Member, IEEE, Aflexible Active and Reactive Power Control Strategy for a Variable Speed Constant Frequency Generating System "IEEE Transactions On Power Electronics,Vol.10,No.4,July 1995pp.110-214.