

HETEROTIC STUDIES FOR YIELD AND ITS RELATED TRAITS IN PEARL MILLET (*Pennisetum glaucum*(L.) R. Br.)

ABSTRACT

The present study was conducted on six parents and eighteen hybrids developed at ICAR Indian institute of millets reaserch, rajendranagar, hyderabad, for sixteen characters. ANOVA revealed significant difference among genotypes for all characters studied. In the present investigation eighteen crosses generated by Line \times Tester mating design were evaluated and heterosis estimated. Heterosis studies helps in finding out superior hybrids over mid parent (Average heterosis), better parent (heterobeltiosis) and standard check (economic heterosis). Among all the crosses studied four crosses *viz.*, 291A X 23S216, 291A X 23S168, 291A X 23S156 and 291A X 23S224 were found as the best performing hybrids for grain yield and its component traits.

Key words : Average heterosis, Heterobeltiosis, Economic heterosis

INTRODUCTION

Pearl millet was domesticated in Africa (west of the Nile), nearly 3000 to 5000 years ago and subsequently spread to southern Asia (Brunkenet *al.*, 1977). It belongs to the family Poaceae (Gramineae), subfamily Panicoideae with chromosome number $2n=14$. Other names of bajra are cat tail, spiked or bulrush millet, cumbu and locally known as bajra or bajari, in telugu it is called as 'sajjalu'. Nearly around 90 million people living in semi-arid and arid climates eat pearl millet as staple food. The utility of pearl millet varies, ranging from food and feed, through forage, fodder, building material, brewing and biofuel, making it an important crop species for food and livelihood security for millions of poor and nutritionally insecure people around the world. In view of climate change, depleting water resources, burgeoning population and widespread malnutrition, there is a need to accelerate the rate of genetic gains in pearl millet. Pearl millet being a highly cross pollinated crop, efficient exploitation of heterosis leads to

higher genetic gains. Pearl millet breeding in India has historically evolved very comprehensively from open-pollinated varieties to hybrid breeding. Hybrid breeding in bajra started with the development of a commercially and economical viable male-sterile line, i.e., Tift 23A. It was developed in the early 1960s in Tifton, Georgia, USA. These provided a breakthrough in the development of hybrids worldwide. Tift 23A was extensively used at Punjab Agricultural University (PAU) Ludhiana India, led to development of the first single-cross pearl millet hybrid, named Hybrid Bajra 1 (HB 1) and other hybrids (HB series). In 1970 downey mildew epidemic resulted due to continuous use of Tift 23 A. It led to diversification of parental lines. The accomplishments of pearl millet breeding are often referred to as one of the greatest success stories in Indian agriculture. There is a considerable scope to further accelerate the genetic gains with hybrid breeding.

MATERIALS AND METHODS

Eighteen crosses along with nine parents 247B, 275B, 292B, 23S110, 23S156, 23S168 and 23S216 developed at ICAR Indian institute of millets research, rajendranagar, hyderabad, and two(2) checks HHB 67 Improved and Pratap were evaluated during *rabi*, 2023 in Randomized Block Design replicated over three replications at Wet land farm, S.V. Agricultural college, Tirupati. Each entry was sown in one row of 3m length at a spacing of 45 cm between the rows and 15 cm between the plants in a row. The recommended dose of N, P and K were applied @ 60:30:20 kg ha⁻¹. The entire P and K and half dose of nitrogen were applied as basal, while remaining nitrogen is applied at 30 days after sowing. Intercultural operations and irrigation schedules were followed as and when necessary. Need based plant protection measures were adopted to raise healthy crop. The mean values were subjected to statistical analysis as suggested by Snedecor and Cochran (1967) and mid parent, better parent and economic heterosis was estimated.

RESULTS

Replicated mean data for the 16 characters studied were subjected to analysis of variance presented in the Table 1, revealed that mean sum of squares of the genotypes

were highly significant for the characters studied indicating the existence of sufficient variability among genotypes for all the characters.

Heterosis studies help in finding out superior hybrids over mid parent (Average heterosis), better parent (heterobeltiosis) and standard check (economic heterosis). In the present investigation eighteen crosses generated by Line \times Tester mating design were evaluated and heterosis estimated and presented in Table 2.

Heterosis studies revealed that, out of eighteen hybrids studied two hybrids (246A \times 23S224) and (274 \times 23S224) recorded highest significant negative heterosis over mid parent, better parent, and standard check pratap and non significant negative heterosis over HHB 67 Improved for days to 50% flowering.

Four hybrids 291A \times 23S216, 291A \times 23S168, 291A \times 23S156 and 291A \times 23S224 out of eighteen hybrids registered significant positive heterosis over mid parent, better parent, and standard checks HHB67 Improved, and non significant positive heterosis over pratap for grain yield.

Hybrid 291A \times 23S216 recorded significant positive heterosis over mid parent, better parent and standard checks HHB67 Improved and pratap for grain yield. Along with grain yield 291A \times 23S216 also recorded significant positive heterosis for SCMR, plant height, panicle length, panicle girth and fodder yield.

Another hybrid 291A \times 23S168, recorded significant positive heterosis over mid parent, better parent and standard check HHB 67 Improved and positive heterosis over pratap for grain yield. Along with grain yield 291A \times 23S168 also recorded positive significant heterosis for plant height, leaf length, panicle length and fodder yield. The results are in agreement with Vetriventhan *et al.* (2008), Bachkaret *et al.* (2014), Jog *et al.* (2014), Bhuri Singh *et al.* (2015), Salagarkar and Wali (2016), Acharya *et al.* (2017), Sumathi and Revathi (2017), Gupta *et al.* (2018), Athoniet *et al.* (2022) and Choudary *et al.* (2023).

Among all the crosses studied four crosses viz., 291A X 23S216, 291A X 23S168, 291A X 23S156 and 291A X 23S224 were found as the best performing hybrids for grain yield and its component traits. These hybrids can be tested in multi location trails for their performance and may be released if found suitable.

DISCUSSION AND CONCLUSION

The general expectation of hybrid breeding is to develop hybrids that are superior than the available standard hybrids which are grown widely. So, there is a need to evaluate the newly developed hybrids with standard hybrids. Hence, hybrids in the current study were evaluated with HHB67 Improved and Pratap. Hybrid 291A X 23S216 recorded significant positive standard heterosis for majority of characters studied i.e., SCMR, plant height, panicle length, panicle girth and fodder yield and grain yield and other hybrid 291A X 23S168 recorded significant positive standard heterosis for plant height, leaf length, panicle length and fodder yield. From all the hybrids studied 291A X 23S216 identified as best cross for grain yield and its component traits.

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5	91A X 23S222	1.67	0.67	9.37	02.47	5.00	.13	41.46	.73	4.16	.61	9.87	.47	.40	7.70	2.63	0.26
6	46A x 23S224	4.67	6.00	3.93	14.50	8.33	.27	12.80	.20	0.16	.39	6.80	.73	.28	7.53	9.22	4.53
7	74A X 23S224	4.67	6.00	2.93	42.27	9.67	.67	19.13	.80	9.80	.24	5.23	.83	.11	8.73	0.37	3.47
8	91A X 23S224	9.00	6.67	5.20	04.60	8.33	.33	36.67	.46	5.03	.89	7.50	.20	2.31	9.03	0.46	4.67
ean		9.52	8.78	0.61	04.24	4.83	.90	29.97	.81	1.57	.59	0.68	.09	.60	7.05	6.88	9.28

DFF - Days to 50 % flowering, DM - Days to maturity, NPT - No of productive tillers per plant, PL - Panicle length, PG - Panicle girth, FLL - Flag leaf length, FLW - Flag leaf width, SCMR - SPAD chlorophyll meter reading SLA - Specific leaf area, LL - Leaf length LW- Leaf width PH - Plant height, FY - Fodder yield, GW - Grain weight, HI - Harvest index, GY - Grain Yield.

Table 2 Mid parent, Better parent and Standard heterosis of the hybrids for all the characters studied

		D				D			
		ays to 50 % flowering				ays to maturity			
		id	etter	HB 67	ratap	id	etter	HB 67	ratap
	46A*23S110	10.85 **	10.85 **	.49 *	8.00 *	5.98 **	8.43 **	.79	8.80 **
	74A*23S110	7.81 *	8.53 *	1.32 **	5.6	4.51 *	6.43 **	.02	6.80 **
	91A*23S110	9.93 **	16.99 **	9.81 **	.6	13.42 **	21.94 **	.04 **	3.2
	46A*23S156	8.95 **	9.30 **	0.38 *	6.4	2.11	2.52	.57	7.20 **
	74A*23S156	9.80 **	10.16 **	.49 *	8.00 *	1.47	1.67	.91	6.00 **
	91A*23S156	13.88 **	20.92 **	4.15 **	3.2	13.14 **	23.23 **	.25 *	4.80 *

	46A*23S168	7.12 *	10.14 **	6.98 **	0.8	0.41	3.2	.04 **	3.2
	74A*23S168	9.43 **	13.04 **	3.21 **	4	2.66	4.80 *	.25 *	4.80 *
	91A*23S168	9.97 **	14.38 **	3.58 **	.8	10.00 **	18.71 **	2.50 **	.8
0	46A*23S216	15.18 **	15.50 **	.83	12.80 **	2.09	3.31	.46	6.40 **
1	74A*23S216	10.59 **	10.94 **	.55	8.80 *	3.53	4.13	.57	7.20 **
2	91A*23S216	14.59 **	21.57 **	3.21 **	4	15.22 **	24.52 **	.46	6.40 **
3	46A*23S222	3.42	5.22	9.81 **	.6	.04	1.21	.93 **	2.4
4	74A*23S222	3.45	5.97	8.87 **	.8	0.41	2.02	.04 **	3.2
5	91A*23S222	12.89 **	18.30 **	7.92 **		13.11 **	21.94 **	.04 **	3.2
6	46A*23S224	16.80 **	19.38 **	1.89	16.80 **	4.80 *	6.17 **	.79	8.80 **
7	74A*23S224	16.13 **	18.11 **	1.89	16.80 **	5.39 **	6.17 **	.79	8.80 **
8	91A*23S224	14.60 **	23.53 **	0.38 *	6.4	16.82 **	25.81 **	.68	8.00 **
	E	.26	.45	.45	.45	.57	.82	.82	.82
		S				SLA			
		CMR							
		id	etter	HB 67	ratap	id	etter	HB 67	ratap
	46A*23S110	15.99 **	16.38 *	4.64	9.02	18.27 *	24.32 **	7.56	.78
	74A*23S110	.82	.11	3.09	.89	7.39	12.84	9.3	.78
	91A*23S110	3.09	9.11	.68	2.04	2.76	8.57	4.86	.86
	46A*23S156	16.16 *	21.23 **	10.17	14.3	13.36	19.78 *	2	2.13
	74A*23S156	6.19	10.03	1.78	6.3	2.76	8.48	4.76	.97
	91A*23S156	.14	.43	.69	.69	10.22	15.59	12.16	.51

	46A*23S168	2.71	7.25	.77	.91	12.7	16.66 *	.81	6.49
	74A*23S168	8.44 **	5.31 *	5.88 **	0.09 **	.64	7.17	.11	7.98
	91A*23S168	7.91 **	5.36 *	9.27 *	3.79	9.44	17.38	8.22	.01
0	46A*23S216	.41	3.44	0.11	.05	5.92	18.81 *	0.83	3.48
1	74A*23S216	.27	.13	1.48	.36	0.4	.51	0.38	3.98
2	91A*23S216	7.75 **	5.14 **	3.80 **	8.10 *	0.76	2.36	10.54	.36
3	46A*23S222	2.45 *	0.28	5.76 **	9.98 **	.65	7.02	3.59	9.97 *
4	74A*23S222	5	5.21	.93	0.85	5.38	5.91	12.63	0.04
5	91A*23S222	.6	3.36	.95	.08	.8	.09	2.41	1.66
6	46A*23S224	3.26	15.60 *	3.75	8.17	1.46	10.73	.05	4.77 *
7	74A*23S224	5.72 *	.89	2.31	.15	1.89 **	6.62 **	5.49 **	5.03 **
8	91A*23S224	.15	0.42	1.49	6.02	.43	.45	0.38	3.98
E		.72	.29	.29	.29	.80	0.16	0.16	0.16
		L				L			
		eaf length				eaf width			
		id	etter	HB 67	ratap	id	etter	HB 67	ratap
	46A*23S110	3.7	6.40 *	.54	20.95 **	0.61	1.22		19.80 **
	74A*23S110	.45	.69	.19	18.92 **	3.49	7.78	0.67 *	17.82 **
	91A*23S110	.99	8.00 **	2.12 **	6.76 *		9.80 *	2.67 **	8.91 *
	46A*23S156	.58	4.79	3.01 **	6.08 *	3.33	12.12 **	6.00 **	13.86 **
	74A*23S156	.38 *	6.16 *	1.24 **	7.43 **	.53	4.04	6.67 **	5.94
	91A*23S156	.05	.67	6.28 **	.05	.49		6.00 **	.99

	46A*23S168		6.90 *	9.47 **	8.78 **	3.61	5.88	.67	20.79 **	
	74A*23S168	.88 **	2.76	4.78 **	4.73	4	6.67	2.00 *	16.83 **	
	91A*23S168	.47 **	.67 *	1.59 **	.11 **	2.67	10.78 **	1.33 **	9.90 *	
0	46A*23S216	2.72	5.3	0.62 **	15.54 **	7.87 *	15.46 **	.33	18.81 **	
1	74A*23S216	.44	4.55	1.50 **	14.86 **	11.23 **	14.43 **	0.67 *	17.82 **	
2	91A*23S216	.55	2.67	9.20 **	1.35	14.57 **	16.67 **	3.33 *	15.84 **	
3	46A*23S222	.56	0.76	5.04 **	12.16 **	.27	5.26	0.00 **	10.89 **	
4	74A*23S222	3.47 **	.11 *	3.01 **	6.08 *	3.78	6.32	8.67 **	11.88 **	
5	91A*23S222	3.91	10.00 **	9.47 **	8.78 **	4.57	7.84 *	5.33 **	6.93	
6	46A*23S224	5.74 *	8.00 *	.77	22.30 **	15.00 **	16.05 **	9.33	32.67 **	
7	74A*23S224	.15		.31	19.59 **	5.33	11.11 *	.67	20.79 **	
8	91A*23S224	.81 **	3.33	8.32 **	2.03	0.50 **	1.96	3.33 **	0.99	
	E	.07	.24	.24	.24	.11	.13	.13	.13	
			P				N			
			lant height				PT			
		id	etter	HB 67	ratap	id	etter	HB 67	ratap	
	46A*23S110	8.14 **	1.54 **	.63	4.71	6.67 **	0.51 **	6.88 **	0.77 **	
	74A*23S110	0.51 **	7.63 **	.78	.06	.82	5.13	5.63 *	2.31 **	
	91A*23S110	0.62 **	7.07 **	1.92 **	3.19 *	22.39 **	33.33 **	18.75 **		
	46A*23S156	1.83 **	.29	7.57 **	8.44 **	13.21	28.13 **	28.13 **	11.54	
	74A*23S156	7.10 **	.09	6.16 **	7.12 **	4.75 *	.38	.38	4.62 **	
	91A*23S156	3.91 **	7.51 **	8.43 **	8.52 **	40.00 **	43.75 **	43.75 **	30.77 **	
	46A*23S168	8.23 **		4.70 **	5.78 **	6.12	17.86 *	28.13 **	11.54	

	74A*23S168	0.80 **	.85	0.46 **	1.12 **	26.32 **	27.59 **	34.38 **	19.23 *
	91A*23S168	3.63 **	5.60 **	9.16 **	8.48 **	7.86 **	7.86 *	.13	6.92 **
0	46A*23S216	6.02 **	.66	9.92 **	1.34 *	5.45	23.53 **	18.75 **	
1	74A*23S216	8.53 **	.53	5.51 **	6.53 **	23.81 **	29.41 **	25.00 **	7.69
2	91A*23S216	1.40 **	5.57 **	3.89 **	3.59 **	38.71 **	44.12 **	40.63 **	26.92 **
3	46A*23S222	3.52 **	1.95 *	5.26 **	6.29 **	9.73 **	4.29	25.00 **	7.69
4	74A*23S222	4.79 **	.41	0.18 **	1.58 *	5.56	10.34	18.75 **	
5	91A*23S222	5.81 **	1.88 **	6.38 **	6.61 **	8.18 *	7.14	18.75 **	
6	46A*23S224	0.58 **	9.75 **	.74	.95	0.00 **	3.48 **	.13	6.92 **
7	74A*23S224	3.91 **	6.47 **	4.85 *	.62	.85	6.9	15.63 *	.85
8	91A*23S224	6.59 **	5.08 **	1.75 **	2.32 **	13.73	21.43 **	31.25 **	15.38
	E	.20	.99	.99	.99	.12	.14	.14	.14

		P				P			
		anicle length				anicle girth			
		id	etter	HB 67	ratap	id	etter	HB 67	ratap
	46A*23S110	6.65 **	5.27 **	2.84 *	8.84 *	.65	.81	3.23 **	15.28 **
	74A*23S110	0.14	8.32	.8	15.34 **	6.67 **	.17	5.82 **	20.37 **
	91A*23S110	6.36 **	0.93	4.74 **	.84 *	.76 *	2.26	0.98 **	9.95 **
	46A*23S156	.87 *	7.39	9.26 **	.42	.56	2.16	7.37 **	5.56
	74A*23S156	.98	4.52	3.26 **	.65	5.42 **	5.52	2.66 **	8.80 *
	91A*23S156	3.37 **	1.92 **	6.21 **	6.19 **	.01	.6	5.45 **	

	46A*23S168	.83	17.60 **	7.16 **	.72	.39	.25	2.56 **	15.74 **
	74A*23S168	1.44 **	3	9.68 **	0.92 **	1.80 **	.48	7.27 **	12.50 **
	91A*23S168	3.71 **	.96 *	5.05 **	3.33 **	.77	.01	5.35 **	6.94
0	46A*23S216	1.70 **	.17	3.58 **	0.17	0.31 **	.39 *	3.33 **	8.33 *
1	74A*23S216	0.89 **	.83	1.79 **	.46	9.48 **	.59	6.26 **	13.19 **
2	91A*23S216	3.38 **	7.65 **	0.00 **	9.25 **	9.21 **	3.82 **	2.53 **	.86
3	46A*23S222	7.65 **	2.24 **	0.74 **	.61	.82	.37	8.62 **	11.57 **
4	74A*23S222	7.41 **	3.63 **	9.89 **	.93	5.06 **	.92	3.00 **	8.56 *
5	91A*23S222	5.65 **	2.23 **	2.63 **	3.30 **	.62	1.51	1.99 **	9.26 *
6	46A*23S224	7.82 **	.65	7.37 **	.89	.99	.56	0.54 **	17.13 **
7	74A*23S224	.51	.69	5.05 **	.02	.61	4.82	3.13 *	22.22 **
8	91A*23S224	4.34 **	6.25 **	8.11 **	7.72 **	5.58 **	.05 *	6.13 **	.46
E		.72	.84	.84	.84	.09	.10	.10	.10

		F				F			
		lag leaf length				lag leaf width			
		id	etter	HB 67	ratap	id	etter	HB 67	ratap
	46A*23S110	7.16	15.19	.9	17.35 *	.14	4.35	5.79 *	16.19 **
	74A*23S110	.61	0.24	.02	19.61 *	4.71	12.90 *	.58	22.86 **
	91A*23S110	.82	7.62	7.89 **	0.2	.2	6.6	0.26 **	5.71
	46A*23S156	6.08	6.22	7.46	8.33	.04	3.85	1.58 **	4.76
	74A*23S156	2.05	11.33	1.06	13.33	2.54	7.69	6.32 **	8.57

	91A*23S156	.24	0.73	7.44 **	.25	0.95	1.89	6.84 **	0.95
	46A*23S168	16.63 *	19.74 **	.29	15.49 *	5.03	7.61	1.84	19.05 **
	74A*23S168	.18	5.21	7.89 **	0.2	1.11	4.3	7.11 *	15.24 **
	91A*23S168	2.21	3.45	3.67 **	.31	3.63	12.26 *	2.37 **	11.43 *
0	46A*23S216	1.99	6.04	7.34	8.43	10.05	12.37 *	1.84	19.05 **
1	74A*23S216	.95	1.97	2.31	12.35	5.26	7.22	8.42 *	14.29 *
2	91A*23S216	.97	4.08	2.79 **	.63	.49	3.77	4.21 **	2.86
3	46A*23S222	.12	0.2	4.62 *	2.75	.74	.26	5.00 **	9.52
4	74A*23S222	2.25	10.33	.05	14.90 *	.26	.23	6.32 **	8.57
5	91A*23S222	13.43 *	18.69 **	2.56	12.16	.33	1.89	6.84 **	0.95
6	46A*23S224	7.21	19.11 *	.01	21.18 **	1.2	10.87	.89	21.90 **
7	74A*23S224	2.13	6.31	4.9	25.78 **	.8	8.6	1.84	19.05 **
8	91A*23S224	10.37	25.14 **	.64	19.12 *	.67	9.43	6.32 **	8.57
	E	.15	.48	.48	.48	.16	.18	.18	.18
		F				1			
		odder yield				000 - grain weight			
		id	etter	HB 67	ratap	id	etter	HB 67	ratap
	46A*23S110	0.89 **	7.46 **	0.91	14.12	.11	6.78	18.32 **	12.23 *
	74A*23S110	2.27 **	8.97 **	.23	18.52 *	7.86	18.79 **	29.37 **	24.11 **
	91A*23S110	5.64 **	2.85 *	2.67 **	.73	7.18	13.20 *	33.83 **	28.90 **
	46A*23S156	4.90 **	2.75 **	3.00 *	4.76	0.34	0.56	12.87 *	6.38
	74A*23S156	1.54 **	6.72 **	6.19 **	2.29	4.38 *	.42	10.07 *	3.37

	91A*23S156	0.09 **	2.27 *	2.04 **	.24	.35	2.6	25.74 **	20.21 **
	46A*23S168	5.22 *	.26	9.57	29.98 **	8.09	16.57 **	26.90 **	21.45 **
	74A*23S168	3.48 **	5.15 **	0.80 **	.28	7.08 **	.64	7.26	0.35
	91A*23S168	10.06 **	7.02 **	01.97 **	6.38 **	3.74 *	0.17	16.01 **	9.75
0	46A*23S216	7.97 **	4.2	.76	18.88 *	1.32 *	0.94	13.20 *	6.74
1	74A*23S216	5.84 **	3.11 **	2.10 *	5.45	4.97 **	1.57 *	2.97	.26
2	91A*23S216	1.90 **	8.21 **	1.65 **	0.65 **	8.95 **	2.77	14.03 **	7.62
3	46A*23S222	4.00 **	.27	.31	16.91 *	6.83	11.91 *	13.37 **	6.91
4	74A*23S222	20.31 *	29.99 **	29.97 **	45.78 **	11.49 *	16.61 **	17.99 **	11.88 *
5	91A*23S222	6.31 *	2.02	0.97 *	6.33	.38	10.91 *	12.38 *	5.85
6	46A*23S224	25.91 **	4.39 **	.86	18.81 *	.91	0.94	13.20 *	6.74
7	74A*23S224	2.24 **	6.16	12.05	31.90 **	4.69 **	.64	7.26	0.35
8	91A*23S224	51.91 **	4.10 **	7.21 **	7.21 **	4.81 **	3.59 **	5.78	.24
E		.57	.65	.65	.65	.85	.98	.98	.98
H					G				
arvest index					rain yield				
	id	etter	HB 67	ratap	id	etter	HB 67	ratap	
	46A*23S110	5.11	13.46 **	1.48 *	9.95 *	2.87 **	6.67 *	3.80 **	45.09 **
	74A*23S110	4.83 **	.35	0.76 *	10.53 *	0.16 **	8.67	5.35 *	48.55 **
	91A*23S110	.68	.9	3.01 *	8.71 *	4.83 **	7.27 **	7.46 **	27.17 **
	46A*23S156	18.61 **	29.50 **	4.00 **	.16	0.05 **	2.22	5.92 **	23.70 **
	74A*23S156	1.98 **	16.39 **	7.05 **	8.79 **	8.61 **	3.70 **	35.21 **	3.47
	91A*23S156	5.56	23.85 **	3.93 **	.19 *	0.68 **	9.26 **	64.79 **	.67

	46A*23S168	7.52 *	12.50 **	6.34 **	.05	.15	23.64 **	7.46 **	27.17 **
	74A*23S168	0.39 **	2.38 **	2.26 **	1.07 **	4.84 **	.82	36.62 **	2.89
	91A*23S168	7.94 *	19.63 **	6.05 **	6.26	1.67 **	3.33 **	63.38 **	.09
0	46A*23S216	.72	0.05	8.76 **	.01	0.40 **	.92	5.77 **	19.65 **
1	74A*23S216	.75	10.12 *	4.02 **	7.90 *	9.56 **	2.31	8.87 **	26.59 **
2	91A*23S216	0.53 **	.2	9.65 **	.73	9.04 **	7.69 **	88.73 **	8.50 **
3	46A*23S222	.71	4.43	6.04 **	7.97 **	3.93 **	.48	16.90 **	10.98 *
4	74A*23S222	6.59 **	4.90 **	5.59 **	1.84 **	4.55 **	.79	15.49 **	11.56 *
5	91A*23S222	9.93 **	23.21 **	7.34 **	5.21	4.08 **	.11	14.08 **	12.14 *
6	46A*23S224	8.09 **	20.84 **	1.12 **	4.00 **	0.54 **	0.1	3.52 **	36.99 **
7	74A*23S224	.62 **	18.51 **	5.26 **	7.34 **	3.77 **	.02	2.25 **	41.62 **
8	91A*23S224	.79	18.35 **	5.56 **	7.58 **	6.87 **	6.87 **	60.56 **	.94
E		.15	.33	.33	.33	.89	.03	.03	.03

* significant at p = 0.05 level, ** significant at p = 0.01 level SE - Standard error

PROPERTY