

## Commentary

### **A Review on the Shrinkage Properties of Concrete**

**Abstract:** This paper provides a comprehensive review of the basic concepts of concrete shrinkage, including plastic shrinkage, temperature shrinkage, carbonation shrinkage, drying shrinkage, and autogenous shrinkage. It also discusses the causes, influencing factors, and control measures of these shrinkage types in detail. Among them, drying shrinkage, which is the most important volume stability deformation of concrete, has its mechanism deeply explored, including the theory of capillary tension, the theory of separation pressure, the theory of solid surface tension, and the theory of interlayer water loss. In addition, the paper also pays attention to the research status of drying shrinkage of mechanism sand concrete, especially the influence of stone powder content, MB value (methylene blue value), mud powder content, and the influence of mineral powder and fly ash on the early shrinkage performance of mechanism sand concrete.

**Keywords:** concrete shrinkage, drying shrinkage, manufactured sand concrete, aggregate characteristics

#### **1 Introduction**

Concrete, as an indispensable material in modern construction, plays a crucial role in ensuring the safety and durability of buildings through its stable and reliable performance. However, the shrinkage behavior of concrete has always been one of the focal issues in both engineering and academic circles. Concrete shrinkage refers to the volume reduction caused by the loss of internal moisture due to factors such as drying, chemical reactions, and temperature changes during setting, hardening, and use. This volume change can not only affect the mechanical properties and durability of concrete but also lead to structural cracking, thereby compromising the overall safety of buildings.

Therefore, conducting in-depth research on the shrinkage behavior of concrete and exploring its mechanisms and influencing factors are of great significance for improving the quality and performance of concrete materials and ensuring the safety and durability of buildings. This paper aims to reveal the laws and characteristics of concrete shrinkage behavior through a systematic review of theoretical analysis, providing a scientific basis and technical support for the optimal design and construction of concrete materials. Additionally, this paper will focus on the mechanisms of concrete drying shrinkage and the current research status of drying shrinkage in manufactured sand concrete, offering valuable references and guidance for engineering practice.

#### **2 Basic Concepts of Concrete Shrinkage**

The phenomenon of concrete undergoing volume reduction due to factors such as changes in water content, chemical reactions, and temperature decreases is collectively referred to as concrete shrinkage. It is a deformation

that is independent of load and related to time, mainly including plastic shrinkage, thermal shrinkage, carbonation shrinkage, drying shrinkage, and autogenous shrinkage<sup>0</sup>.

## **2.1 Plastic Shrinkage**

Plastic shrinkage of concrete refers to the volume change that occurs in freshly poured concrete before it hardens. Plastic shrinkage typically occurs during the construction process, especially within 3 to 12 hours after concrete pouring. During this period, the cement hydration reaction is intense, molecular chains are gradually formed, and there is bleeding and rapid evaporation of water within the concrete, leading to water loss and shrinkage. Additionally, as aggregates sink due to their own weight and the concrete has not fully hardened, this type of shrinkage is termed plastic shrinkage.

Plastic shrinkage is related to the composition of concrete materials, external environmental conditions, and construction techniques. Specifically, factors such as high cement content, high water-cement ratio, large exposed surface area, low environmental humidity, and high wind speed can all contribute to increased plastic shrinkage in concrete.

When plastic shrinkage is constrained by external factors (such as formwork, steel reinforcement, or other concrete components), tensile stresses are generated within the concrete, which may lead to uneven stress distribution within the concrete structure and stress concentration in certain areas. Over time, this uneven stress distribution can further exacerbate deformation and damage to the concrete structure, affecting the overall stability of the structure.

To mitigate plastic shrinkage, it is important to ensure that the concrete is vibrated uniformly and compactly, avoiding over-vibration or insufficient vibration. Additionally, the support and stability of the formwork should be enhanced to prevent swelling or settlement. Measures such as covering the concrete surface with plastic film or spraying a curing agent before initial setting should be taken to maintain the necessary humidity on the concrete surface and prevent excessive water evaporation that can cause plastic shrinkage. The curing time should be sufficient to ensure that the concrete fully hardens and reaches the designed strength.

## **2.2 Thermal Shrinkage**

Concrete thermal shrinkage, also known as cold shrinkage, is the deformation that occurs in concrete due to temperature decrease (above 0°C) during its setting, hardening, and use. After concrete pouring, the cement hydration reaction releases heat, raising the internal temperature of the concrete. As the cement hydration reaction progresses, the heat gradually dissipates, causing the internal temperature of the concrete to decrease and resulting in volume reduction, known as thermal shrinkage. When the external ambient temperature is low, the concrete surface cools and shrinks rapidly, while the interior remains at a higher temperature due to the hydration heat, leading to differences in temperature and shrinkage between the interior and exterior. For mass concrete, cracks are mainly caused by thermal shrinkage.

Proper curing conditions are crucial for controlling concrete thermal shrinkage. Adequate curing can slow down the evaporation rate of water from the concrete surface, reduce temperature gradients and shrinkage differences, and thereby minimize crack formation. In design, it is advisable to prioritize the use of cement types

with low hydration heat and low shrinkage, such as moderate heat cement or low heat cement. These cement types release less heat during the hardening process, reducing the temperature stresses within the concrete and thus decreasing thermal shrinkage.

### **2.3 Carbonation Shrinkage**

Concrete carbonation shrinkage refers to the phenomenon of volume reduction that occurs when carbon dioxide (CO<sub>2</sub>) in the atmosphere reacts with the hydration products of cement in the presence of moisture (actually, the true mediator is carbonic acid), producing calcium carbonate (CaCO<sub>3</sub>) and free water, among other products. Carbonation shrinkage primarily arises from the chemical reactions between CO<sub>2</sub> and the hydration products of cement. These reactions include the reaction of Ca(OH)<sub>2</sub> with CO<sub>2</sub> to form CaCO<sub>3</sub>, which leads to volume contraction. Additionally, the carbonation of Ca(OH)<sub>2</sub> reduces the alkalinity of the cement paste, causing other originally stable hydration products to also undergo carbonation reactions, further exacerbating volume contraction.

Dense concrete structures can slow down the diffusion rate of CO<sub>2</sub>, thereby reducing the rate of carbonation. A moderate humidity level (approximately 50%) favors the carbonation process. Excessively high humidity fills the pores of the concrete with water, hindering the diffusion of CO<sub>2</sub>. Conversely, excessively low humidity results in insufficient water in the pores for CO<sub>2</sub> to form carbonic acid, making carbonation less likely to occur.

### **2.4 Drying Shrinkage**

Drying shrinkage of concrete refers to the irreversible deformation that occurs when concrete, after cessation of curing, loses its adsorbed water within the internal capillary and gel pores when exposed to unsaturated air. This type of shrinkage is caused by the migration of water within the concrete and pore characteristics, and it is one of the main factors influencing concrete shrinkage.

A higher water-cement ratio results in greater drying shrinkage of concrete. Additionally, the content and type of aggregates also affect drying shrinkage. A higher aggregate content leads to less drying shrinkage, and different types of aggregates have varying effects on drying shrinkage. Aggregates with good grading or increased maximum particle size have lower porosity, which reduces the drying shrinkage of concrete. Relative humidity has a significant impact on the drying shrinkage of concrete. In environments with lower relative humidity, the evaporation rate of water from the concrete surface increases, leading to greater drying shrinkage.

The volume of cement hydration products is smaller than the total volume of cement and water before the reaction, which is one of the main reasons for volume shrinkage in concrete. Different types of cement have different hydration reaction characteristics and products, which have varying effects on the drying shrinkage of concrete. For pure Portland cement, the shrinkage of cement paste mainly depends on the content of tricalcium aluminate (C<sub>3</sub>A), sulfur trioxide (SO<sub>3</sub>), gypsum, and cement fineness. Generally, shrinkage increases with the content of C<sub>3</sub>A mineral components, and cement with finer particle size and insufficient gypsum content also exhibits greater shrinkage.

### **2.5 Autogenous Shrinkage**

Autogenous shrinkage of concrete refers to the self-volume deformation that occurs due to the consumption of water during cement hydration under sealed conditions (without moisture exchange with the outside environment). During this process, the consumption of water during cement hydration causes the liquid level in the gel pores to drop, forming a meniscus, which produces the so-called self-drying effect. This leads to a decrease in the relative humidity of the concrete and a reduction in volume <sup>[2][3]</sup>.

The water-cement ratio has a significant impact on autogenous shrinkage of concrete. When the water-cement ratio is less than 0.35, the relative humidity of the concrete quickly drops below 80%, at which point autogenous shrinkage and drying shrinkage contribute almost equally. As the water-cement ratio decreases, autogenous shrinkage becomes more pronounced. The elastic modulus, particle size, and content of aggregates also have an impact on autogenous shrinkage. A higher aggregate content and elastic modulus result in less autogenous shrinkage. Aggregates serve as the skeleton of concrete, restricting autogenous shrinkage. Aggregate grading, maximum particle size, ratio of coarse to fine aggregates, and aggregate volume fraction in concrete all affect autogenous shrinkage. Curing conditions also have an impact on autogenous shrinkage. Timely and adequate curing can accelerate cement hydration, but even if water is replenished during curing, autogenous shrinkage may still occur because external water is not easily permeable into the concrete.

Autogenous shrinkage is a special case of drying shrinkage, but they are comparable in magnitude. Autogenous shrinkage mainly occurs in the initial stages after concrete mixing, so most or even all of the autogenous shrinkage of concrete may have already occurred before formwork removal.

### **3 Mechanisms of Drying Shrinkage in Concrete**

Drying shrinkage, as the primary type of shrinkage deformation affecting the volume stability of concrete, accounts for approximately 80% of the total shrinkage deformation in concrete, making it highly representative in the observation and study of volume stability. Concrete operating in a dry environment is prone to drying shrinkage and other shrinkage deformations due to rapid water evaporation rates. Furthermore, for manufactured sand concrete, due to the presence of its own stone powder, internal chemical reaction phenomena such as rapid and concentrated early hydration reactions are observed in practical applications. Therefore, under the coupling effects of the above multiple factors, the drying shrinkage performance of manufactured sand concrete is a continuous and severe challenge <sup>[4]</sup>.

The analysis of microscopic mechanisms has laid a solid foundation for in-depth research on the drying shrinkage of concrete. Currently, the following four theories are generally accepted regarding the mechanisms that cause drying shrinkage in concrete:

#### **3.1 Capillary Tension Theory**

The capillary tension theory, as a fundamental theory in micromechanics, has been a 普遍 explanation for the study of drying shrinkage in concrete. It suggests that drying shrinkage in concrete occurs due to capillary tension arising from partially saturated capillary pores formed within the concrete after the cement hydration reaction, especially when the relative humidity inside the matrix exceeds 45% <sup>[5]</sup>. Research generally agrees that drying

shrinkage is related to changes in the meniscus of water in capillaries during the drying process. As concrete is exposed to a dry environment for an extended period, internal moisture continuously escapes into the surrounding environment, generating an increasingly negative pressure on the capillary walls. Meanwhile, as the relative humidity changes, the vapor pressure above the concave meniscus of the capillary pores also increases. Under the combined action of these forces, capillary water tension increases to maintain internal liquid-level equilibrium, leading to continuous compression of the cement paste in the concrete and resulting in macroscopic volume shrinkage deformation.

### **3.2 Disjoining Pressure Theory**

This theory proposes that when the gap between the surfaces of adjacent particles within the paste reaches a certain distance, the water adsorbed on the surfaces of the solid particles generates an attractive force, known as disjoining pressure. When the adsorbed water within the concrete evaporates and escapes in a dry environment, it causes a decrease in the relative humidity between the particles. Studies have shown that when the relative humidity of the interlayer water is less than 35%, the disjoining pressure at this point will be smaller than the van der Waals force <sup>[5]</sup>. Consequently, the gaps between the gel particles decrease, and the particles pack more tightly together, leading to the occurrence of drying shrinkage.

### **3.3 Surface Tension Theory of Solid Surfaces**

This theory suggests that the drying shrinkage of concrete is caused by the surface tension generated by the water adsorbed on the surfaces of internal gel particles. Specifically, due to differences in the binding forces among water molecules on the particle surfaces, the energy on the particle surfaces is higher than that inside, resulting in surface tension. The surface tension of cement particles in cement paste is related to the relative humidity. Research indicates that a relative humidity of 45% serves as a critical point. When the ambient humidity is above 45%, a large number of water molecules are adsorbed on the surfaces of cement particles, and the surface tension generated between particles is negligible. However, when the humidity of the environment in which the concrete is placed is below the critical value of 45%, to maintain hydrostatic pressure equilibrium inside and outside the particles, the surface tension gradually increases as water evaporates, causing the particles to decrease in volume and resulting in drying shrinkage of the concrete <sup>[6]</sup>.

### **3.4 Interlayer Water Loss Theory**

This theory proposes that the hydrated cement product, C-S-H (Calcium-Silicate-Hydrate) gel, inherently possesses a layered structure. A reduction in the relative humidity within the concrete creates an energy gradient with the external environment, forcing interlayer water to migrate outwardly. Ultimately, this leads to macroscopic and microscopic shrinkage deformation of the concrete. This theory is generally recognized as a primary factor influencing the drying shrinkage of concrete. It is universally believed that interlayer water migration and irreversible shrinkage deformation occur only when the relative humidity is less than 11% <sup>[7]</sup>.

Under such conditions, the interlayer water within the C-S-H gel structure is lost due to drying, causing the gel layers to contract and leading to a reduction in the overall volume of the concrete. This phenomenon is particularly significant in environments with extremely low humidity, where the loss of interlayer water

contributes significantly to the drying shrinkage of concrete.

## **4 Research Status of Drying Shrinkage of Manufactured Sand Concrete**

Manufactured sand, as an artificial sand, boasts a wide range of sources, low cost, and environmental friendliness. As a substitute for natural sand, it offers advantages such as abundant resources, low cost, environmental sustainability, and more. Research on manufactured sand aids in optimizing its production processes, improving product quality, meeting the demand for sand materials in construction projects, while reducing the exploitation of natural resources and promoting green and sustainable development in the construction industry. Its application in construction projects is becoming increasingly widespread. However, there are differences between the characteristics of manufactured sand and natural sand, leading to variations in the properties of their respective concretes. Drying shrinkage is a significant deformation property of manufactured sand concrete after pouring, which directly affects the durability and crack resistance of the concrete. By studying the drying shrinkage of manufactured sand concrete, we can gain a deeper understanding of its shrinkage mechanism and influencing factors, thereby optimizing the concrete mix proportions and enhancing the overall performance of the concrete. Furthermore, studying the drying shrinkage of manufactured sand concrete can further promote the application of manufactured sand and provide technical support for the widespread use of manufactured sand concrete in construction projects.

The primary difference between manufactured sand and natural sand lies in their stone powder content. This section focuses on the impact of stone powder content on the drying shrinkage of manufactured sand concrete.

Malhotra V.M.<sup>[8]</sup> and others found that limestone powder content always benefits the adhesive properties of concrete. Within the range of 0 to 20% incorporation, the drying shrinkage rate increases with the increase of stone powder content, and beyond 10%, the influence of the water-cement ratio becomes greater than that of the stone powder content. Ma et al.<sup>[9]</sup> explored the shrinkage properties of different manufactured sand mortars and found that the manufactured sand mortar made from natural stone has lower drying shrinkage values than that made from recycled aggregates. Li Meili et al.<sup>[10]</sup> conducted experiments on manufactured sand concrete with stone powder contents of 0%, 5%, and 10%. Their research on the shrinkage of manufactured sand concrete revealed that when the stone powder content does not exceed 10%, the shrinkage is hardly affected by the stone powder content.

Wang Jiliang<sup>[11]</sup> studied and concluded that an increase in the MB value of manufactured sand has a significant impact on the drying shrinkage of concrete, especially on its early-age shrinkage. When the MB value of manufactured sand is less than or equal to 1.10, there is basically no effect on the drying shrinkage rate of concrete at 1d and 3d, with a slight increase in the drying shrinkage rate at 5d and beyond. However, when the MB value is greater than or equal to 1.45, there is a noticeable increase in the drying shrinkage rate of concrete, both in the early and later stages, especially in the early stages. When the MB value is greater than or equal to 2.15, the drying shrinkage rates of concrete at 1d and 3d increase by 20% and more than 20% respectively compared to the

control, while the ultimate drying shrinkage rate of the concrete increases by more than 8.8%.

Li Beixing et al.<sup>[12]</sup> studied the impact of the methylene blue (MB) value on shrinkage and found that the presence of clay increases the plastic shrinkage of the concrete surface. Additionally, the drying shrinkage rate of concrete increases as the MB value rises. With an increasing MB value, especially when it is  $\geq 1.45$ , there is a notable increase in the drying shrinkage rate of concrete, both in the early and later stages. The main reason for this is that clay particles, which have a porous layered structure, adsorb a large amount of mixing water and swell when dispersed in concrete. Once the concrete is exposed to a dry environment, as surface water continuously evaporates and is lost, water migrates from the interior of the concrete to the exterior, reducing the internal relative humidity. The water originally adsorbed in the pores of clay particles is released due to diffusion. Furthermore, the presence of clay in manufactured sand, with its large specific surface area, increases the volume content of the paste to a certain extent. Both of these factors contribute to an increase in the degree of drying shrinkage of the concrete.

Hu Bing et al.<sup>[13]</sup> reached a similar conclusion in their research. The drying shrinkage rate of mortar increases with an increase in the mud and fine powder content of manufactured sand, particularly affecting early-age drying shrinkage more significantly. Experimental studies were conducted to investigate the impact of different mud and fine powder contents (0%, 1%, 3%, 5%, and 7%) on the drying shrinkage of mortar. The results showed that as the mud and fine powder content increases, the drying shrinkage value of the mortar also increases, and the drying shrinkage values of all mortar mixes increase with age. The reason for the increase in shrinkage due to mud and fine powder is that the mud and fine powder contained in the mortar are non-reactive substances with very fine particles that adsorb a large amount of water. These non-reactive substances weaken the bond between the cement paste and the aggregates in the interface zone, affecting the adhesion between the paste and the aggregates and reducing the aggregates' ability to inhibit shrinkage. On the other hand, the water adsorbed by them is free water that is easily volatile. After evaporation, their deformation is significant, leading to a more pronounced increase in the drying shrinkage value of mortar with a higher mud and fine powder content compared to mortar with a lower content. Further analysis revealed that at 3 days, the drying shrinkage value of mortar with a mud and fine powder content of 7% increased by up to 64% compared to mortar with a mud and fine powder content of 0%, by 43.9% at 7 days, and by only 28% at 90 days. It can be seen that mud and fine powder have a more significant impact on the early-age drying shrinkage value of mortar.

Yang Haicheng et al.<sup>[14]</sup> studied the impact of granite powder on the performance of C80 high-performance concrete and found that the drying shrinkage rate of manufactured sand concrete is comparable to that of river sand concrete when the granite powder content does not exceed 4.5%. However, when the granite powder content exceeds 6.5%, the drying shrinkage rate increases significantly. As the granite powder content in manufactured sand increases, the drying shrinkage values of high-strength, high-performance concrete at different ages generally show an increasing trend. Specifically, when the granite powder content increases from 3.0% to 6.5%, the 60-day drying shrinkage value of manufactured sand high-strength, high-performance concrete increases from  $246 \times 10^{-6}$ , although the increase is not significant. However, when the granite powder content increases from 6.5% to 8.5%, the 60-day drying shrinkage value of high-strength manufactured sand concrete increases from  $264 \times 10^{-6}$ ,

indicating a significant increase in the drying shrinkage value of the concrete. Therefore, to reduce the drying shrinkage of C80 high-strength manufactured sand concrete, the granite powder content in manufactured sand should not exceed 6.5%. Additionally, compared to concrete made with river sand, when the granite powder content in manufactured sand does not exceed 4.5%, the drying shrinkage value of high-strength manufactured sand concrete is comparable to that of river sand concrete. An appropriate amount of granite powder can optimize the particle distribution of the concrete paste, serving as a micro-aggregate filler, thereby improving the compactness of the concrete and benefiting the reduction of shrinkage deformation in high-strength concrete. However, excessive granite powder content in manufactured sand will increase the proportion of paste in the concrete, thus increasing the drying shrinkage deformation.

Wei Yuanyuan et al.<sup>[15]</sup> studied the shrinkage properties of manufactured sand concrete and found that the total shrinkage value is greater than that of river sand concrete. The shrinkage values of manufactured sand concrete and river sand concrete at the same mix proportions within 90 days were compared. Both types of concrete exhibited increasing shrinkage values as the age increased. Even after 90 days, the shrinkage values continued to increase. Overall, the total shrinkage of manufactured sand concrete is significantly greater than that of river sand concrete. The high content of granite powder in manufactured sand concrete, with small particle sizes, has a significant adsorption effect on pore fluid in the concrete matrix, reducing the internal relative humidity of the concrete and increasing capillary pressure, ultimately leading to increased autogenous shrinkage in manufactured sand concrete.

Imamoto et al.<sup>[16]</sup> studied the impact of aggregate specific surface area on the drying shrinkage of concrete and concluded that the larger the specific surface area of the aggregate, the greater the drying shrinkage rate. The specific surface area of aggregates generally increases as the particle size decreases, consistent with Imamoto's findings. Li Jiazheng et al. pointed out in their research that as the maximum particle size of aggregates decreases, the drying shrinkage rate of ECC gradually increases. Adesina et al.<sup>[17]</sup> studied the shrinkage properties of ECC prepared with waste glass replacing quartz sand and found that glass sand can reduce the shrinkage rate, and 2.0 vol% of PVA fibers can prevent plastic shrinkage cracks.

Li Qian et al.<sup>[18]</sup> investigated the impact of slag powder and fly ash on the early-age shrinkage properties of manufactured sand concrete and found that adding slag powder alone increases early-age shrinkage, and the shrinkage rate gradually increases with age. Adding fly ash alone is better than adding a blend of fly ash and slag powder in terms of early-age shrinkage. Concrete with single additions of Class I fly ash, ground slag powder, or a blend of both exhibits varying degrees of shrinkage, and the shrinkage rate increases with age. Concrete with 30% single addition of ground slag powder exhibits greater shrinkage at all ages compared to concrete with 30% fly ash, with 28-day shrinkage rates of  $373 \times 10^{-6}$ , respectively. When 20% fly ash is blended with 10% ground slag powder, the early-age shrinkage (3 days) of the concrete is reduced compared to single additions, but the later-age shrinkage increases significantly, with the 28-day shrinkage falling between that of single additions of fly ash and ground slag powder. This is because blending fly ash and ground slag powder improves the particle size distribution of the cementitious materials, making the system more dense and reducing the evaporable water

content, which makes water evaporation more difficult and delays the early-age shrinkage rate of the concrete. However, as the curing age increases, the pozzolanic effect of ground slag powder enhances, and its hydration products gradually refine the pores, increasing the capillary negative pressure effect and significantly increasing the later-age shrinkage of the concrete.

## 5 Conclusion

(1) Concrete shrinkage is a complex phenomenon essentially characterized by volume reduction resulting from a combination of factors, including but not limited to water content changes, chemical reactions, and temperature decreases. Specifically, the types of concrete shrinkage include plastic shrinkage, temperature shrinkage, carbonation shrinkage, drying shrinkage, and autogenous shrinkage. These types of shrinkage are closely related to the passage of time and are independent of external loads. Plastic shrinkage is particularly significant in the initial stage after concrete pouring, influenced by factors such as material composition, external environmental conditions, and construction techniques. Temperature shrinkage arises from temperature differences between the interior and exterior of concrete, which is particularly evident in mass concrete. Carbonation shrinkage is the result of reactions between concrete and carbon dioxide in the air, while drying shrinkage is caused by the loss of internal moisture in concrete. Autogenous shrinkage is a special type of shrinkage that occurs under sealed conditions due to volume deformation resulting from the consumption of water during cement hydration.

(2) Drying shrinkage plays a decisive role in the volume stability of concrete. To gain a deeper understanding of this phenomenon, researchers have proposed various theories to explain its mechanism, including capillary tension theory, disjoining pressure theory, solid surface tension theory, and interlayer water loss theory. These theories reveal the volume shrinkage caused by the loss of internal moisture in concrete at the microscopic level, providing a solid theoretical foundation for in-depth studies on the drying shrinkage behavior of concrete.

(3) Manufactured sand, as a widely used substitute for natural sand, plays an important role in construction engineering. However, compared with natural sand concrete, the drying shrinkage performance of manufactured sand concrete exhibits certain differences. Specifically, factors such as stone powder content, MB value (an indicator representing the content of mud and clay substances in manufactured sand), and clay content have significant impacts on the drying shrinkage of manufactured sand concrete. Studies have shown that an appropriate amount of stone powder can optimize concrete performance, but excessive stone powder will lead to increased drying shrinkage. Furthermore, the total shrinkage of manufactured sand concrete is usually greater than that of river sand concrete, which may be related to the adsorption effect of stone powder particles and the specific surface area of aggregates. Therefore, in the application of manufactured sand concrete, it is necessary to reasonably control the stone powder content and optimize the concrete mix proportions to reduce drying shrinkage and thereby improve the overall performance of concrete.

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